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NIXON & VANDERHYE, PC
901 NORTH GLEBE ROAD, 11TH FLOOR
ARLINGTON, VA 22203

EXAMINER	
HINDENLANG, ALISON L	

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BEFORE THE BOARD OF PATENT APPEALS AND INTERFERENCES

Application Number: 10/584,235
Filing Date: September 08, 2006
Appellant(s): SIMMELINK ET AL.

Bryan H Davidson
Reg. No. 30,251
For Appellant

EXAMINER'S ANSWER

This is in response to the appeal brief filed 07/08/2011 appealing from the Office action mailed 11/08/2010.

(1) Real Party in Interest

The examiner has no comment on the statement, or lack of statement, identifying by name the real party in interest in the brief.

(2) Related Appeals and Interferences

The examiner is not aware of any related appeals, interferences, or judicial proceedings which will directly affect or be directly affected by or have a bearing on the Board's decision in the pending appeal.

(3) Status of Claims

The following is a list of claims that are rejected and pending in the application:

Claims 1, 2, 4-8 and 10-15 are rejected and pending, where claims 1 and 14 are independent claims.

(4) Status of Amendments After Final

The examiner has no comment on the appellant's statement of the status of amendments after final rejection contained in the brief.

(5) Summary of Claimed Subject Matter

The examiner has no comment on the summary of claimed subject matter contained in the brief.

(6) Grounds of Rejection to be Reviewed on Appeal

The examiner has no comment on the appellant's statement of the grounds of rejection to be reviewed on appeal. Every ground of rejection set forth in the Office action from which the appeal is taken (as modified by any advisory actions) is being maintained by the examiner except for the grounds of rejection (if any) listed under the

subheading “WITHDRAWN REJECTIONS.” New grounds of rejection (if any) are provided under the subheading “NEW GROUNDS OF REJECTION.”

(7) Claims Appendix

The examiner has no comment on the copy of the appealed claims contained in the Appendix to the appellant’s brief.

(8) Evidence Relied Upon

6448359	Kavesh	9-2002
5296185	Chau	3-1994
4054468	Honnaker	10-1977

(9) Grounds of Rejection

The following ground(s) of rejection are applicable to the appealed claims:

1. Claims 14 and 15 are rejected under 35 U.S.C. 103(a) as being unpatentable over Chau (US 5296185) and optionally further in view of Honnaker (US 4054468) (both of record).

2. With respect to claims 14 and 15, Chau teaches:

Spinplate… comprising

at least 10 spinholes (“the spinneret may contain as many as 100 or 1000 or more" spinholes, column 5, lines 25-26),

wherein each spinhole has a geometry comprising

an inflow zone of constant diameter of at least Do and a length of Lo (“each hole contains: (a) an inlet (10”, column 5, lines 31-32, figure 1)…,

a downstream zone of constant diameter of at least Dn wherein Dn is from 0.3 to 5 mm (in a low draw-small hole process, the capillary section and the ext preferably have an average diameter of no more than about 0.5mm...at least 0.5 mm in diameter...in a high-draw-large hole process... at least about 0.5 mm in diameter...preferably no more than about 5 mm in

diameter...", column 6, lines 14-24) and a length Ln ("a capillary section (9)", column 5, line 36) and a length/diameter ratio Ln/Dn of from 0 to 25 ("the length of the capillary section…is preferably at least about 0.1 times the diameter….is preferably no more than about 10 times the diameter of the capillary", column 5, lines 45-52), and

a contraction zone between the inflow and downstream zones having a gradual decrease in diameter from the diameter Do of the inflow zone to the diameter Dn of the downstream zone ("a transition cone (2) where the hole narrows by and angle (theta) before entry into a capillary", column 5, lines 33-35, figure 1) and a cone angle in the range 8-75°("the angle must be no more than about 60o", column 6, lines 49-50)

3. Chau does not specifically teach a ratio Lo/Do of at least 5. However, Chau further teaches "the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole" (column 6, lines 3-6). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio of the constant diameter zone for the purpose of maximizing flow stability. It has been held that where the general conditions of a claim are disclosed in the prior art, discovering the optimum or workable ranges involves only routine skill in the art. *In re Aller, 105 USPQ 233, 235.*

4. Should applicant wish to argue that the teachings of Chau under *In re Aller* as cited above are insufficient to obviate the claimed Lo/Do ratio the rejection may be considered in view of Honnaker.

5. In the same field of endeavor, spinnerets, Honnaker teaches "typically capillary diameters are 2 to 4 mils (0.05 to 0.10 mm) at L/D ratios of at least about 2.5. Preferably the diameter of the counterbore is from 6 to 12 or more times the diameter of the spinning capillary and the length of the counterbore … is about 2 to 8 times the diameter of the counterbore" (column 4, lines 2-9, figure 2) for the purpose of obtaining filaments with preferred tensile properties from solutions of a given viscosity (column 3,

lines 66-68). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio to at least 5 as taught by Honnaker for the purpose of producing filaments with the desired properties based on solution viscosity.

6. It has been held that the combination of familiar elements according to known methods is likely to be obvious when it does not more than yield predictable results. *KSR Int'l Co. v. Teleflex Inc.,* 82 USPQ2d 1385 (2007).

7. Claims 1, 2, 4-8 and 10-13 are rejected under 35 U.S.C. 103(a) as being unpatentable over Kavesh (US 6448359) further in view of Chau (US 5296185) and optionally in view of Honnaker (US 4054468) (all of record).

8. With respect to claim 1, Kavesh teaches:

Process for making high-performance polyethylene multifilament yarn ("preparing a high tenacity, high modulus multi-filament yarn", column 1, lines 37-39) comprising the steps of

a) making a solution of ultra-high molar mass polyethylene (UHPE) in a solvent ("extruding a solution of polyethylene and solvent", column 1, lines 39-40), wherein the UHPE has an intrinsic viscosity of between 5 and 40 dl/g ("a solution of polyethylene and solvent having an intrinsic viscosity between about 4 dl/g and 40 dl/g", column 1, lines 39-41 and for example "linear polytethylene was Himont UHMW 1900 having an intrinsic viscosity of 18 dl/g", column 6, lines 1-2);

b) spinning of the solution through a spinplate containing a plurality of spinholes into an air-gap to form fluid filaments (through a multiple orifice spinneret into a cross-flow gas stream", column 1, lines 41-42), while applying a draw ratio ("stretching the fluid product", column 1, line 43)... DRag at least 1 ("jet draw must be at least 5:1, and is preferably at least about 12:1", column 5, lines 9-11);

c) cooling the fluid filaments to form solvent-containing gel filaments ("quenching the fluid product in a quench bath...to form a gel product", column 1, line 46-48);

d) removing at least partly the solvent from the filaments ("removing the solvent from the gel product", column 1, line 49); and

e) drawing the filaments in at least one step before, during and/or after said solvent removing, while applying a draw ratio ("stretching the gel product", column 1, line 48) DRsolid of at least 4 (see Table 1, examples 1-5 column "solid state stretch" where all values are above 4), wherein

each of the spinholes has a geometry comprising a contraction zone having a gradual decrease in diameter from a diameter D0 to a diameter Dn ("the spinneret holes 28 should have a tapered entry region 30", column 4, lines 49-50)...

and wherein each of the spinholes comprises a zone downstream of the contraction zone ("the spinneret holds 28 should have a tapered entry region 30 followed by a capillary region of constant cross section 32", column 4, lines 50-52) having a constant diameter Dn of from 0.3 to 5 mm ("the capillary diameter should be 0.2 to 2 mm preferably 0.5 to 1.5 mm", column 4, lines 54-55) and a length Ln with a length/diameter ratio of Ln/Dn of from 0 to at most 25 ("in which the length/diameter (L/D) ratio is more than about 10:1", column 4, lines 52-53)

9. Kavesh does not define a DRfluid as claimed or teach that the spinholes have a constant diameter inflow zone upstream of the contraction zone.

10. In the same field of endeavor, solution spinning spin plates for high viscosity solutions, Chau teaches a spinneret where "each hole contains (a) an inlet (1) (b) optionally, a transition cone (2) where the hole narrows by an angle (theta) before entry into a capillary section" (column 5, lines 31-35, figure 1) for the purpose of maximizing the stability of flow through the spinhole (column 6, lines 3-5) of polymers with viscosities greater than 5dl/g (column 5, lines 21-32). It would have been obvious to one of ordinary skill in the art at the time of the invention to modify the method taught by Kavesh by using a spin plate with an added inlet section upstream of the cone as taught by Chau for the purpose of stabilizing the polymer flow through the spinhole.

11. Chau further teaches that the cone angle of the transition section varies from less than about 90o to less than about 20o depending on shear rate (column 6, lines 46-52).

12. Chau further teaches "the air gap contains a draw zone where the dope is drawn to a spin-draw ratio of at least about 20, preferably at least about 40, more preferably at least about 50, and most preferably at least about 60" (column 7, lines 58-62 – examiner understands this ratio to be DRag of the instant invention).

13. The combination of Kavesh and Chau as above does not explicitly teach a DRfluid as claimed:

at least 50, wherein DRfluid = DRsp X DRag where DRsp is the draw ratio in the spinholes and DRag is the draw ratio in the air-gap, with DRsp greater than 1 and and DRag being at least 1

14. However, DRsp is defined in the specification as DRsp = $(Do/Dn)^2$. Figure 2 of Kavesh clearly shows that the diameter of the spinhole at entry is greater than the diameter of the capillary outlet and Kavesh as cited above specifically teaches “the spinneret holes 28 should have a tapered...region" (column 4, lines 50-51). Thus it would be clear to one of ordinary skill in the art that Kavesh teaches a DRsp greater that 1. Furthermore, Figure 1 of Chau clearly shows that Do – the spinneret entry hole diameter is greater the spinneret capillary outlet and Chau specifically teaches “the hole is preferably broader at the inlet, and becomes narrower through a transition cone within the spinneret to form a capillary section that leads to the exit” (column 5, lines 59-62). Thus it would be clear that Chau teaches a DRsp greater than 1. The combination as above teaches that the DRag must be at least 5 (Kavesh, column 5, lines 9-11) and can be greater than 50 (Chau, column 7, lines 58-62) for the purpose of producing fibers with a desired diameter per filament (Chau, column 7, lines 65-66). It would have been obvious to one of ordinary skill in the art at the time of the invention that the combination teaches a range of DRfluid values which includes the claimed range of at least 50 for the purpose of producing fibers with a desired diameter. Further more it has been held that where the claimed range overlaps or lies inside of a prior art range a prima facie case of obviousness exists. *See In re Werthim, 541 F2d 257, 191 USPQ 90 (CCPA 1976).*

15. The combination does not teach that the Lo/Do ratio of the constant diameter zone is at least 5.

16. Chau further teaches “the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole” (column 6, lines 3-6). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio of the constant diameter zone for the purpose of maximizing flow stability. It has been held that where the general conditions of a claim are disclosed in the prior art, discovering the optimum or workable ranges involves only routine skill in the art. *In re Aller, 105 USPQ 233, 235.*

17. Should applicant wish to argue that the teachings of Kavesh and Chau under *In re Aller* as cited above are insufficient to obviate the claimed Lo/Do ratio the rejection may be further considered in view of Honnaker.

18. In the same field of endeavor, spinhole design, Honnaker teaches “typically capillary diameters are 2 to 4 mils (0.05 to 0.10 mm) at L/D ratios of at least about 2.5. Preferably the diameter of the counterbore is from 6 to 12 or more times the diameter of the spinning capillary and the length of the counterbore ... is about 2 to 8 times the diameter of the counterbore” (column 4, lines 2-9, figure 2) for the purpose of obtaining filaments with preferred tensile properties from solutions of a given viscosity (column 3, lines 66-68). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio in the spin plate of the combination as taught above such that it is at least 5 as taught by Honnaker for the purpose of producing filaments with the desired properties based on solution viscosity.

19. With respect to claim 2, Chau further teaches "the spinneret may contain as many as 100 or 1000 or more" spinholes (column 5, lines 25-26).

20. With respect to claim 4, Chau as applied in the combination above teaches that the cone angle of the transition section varies from less than about 90o to less than about 20o depending on shear rate (column 6, lines 46-52).

21. With respect to claims 5 and 6, Chau as applied in the combination above teaches "the hole is preferably broader at the inlet, and becomes narrower through a transition cone within the spinneret to form a capillary section that leads to the exit" (column 5, lines 59-62) but does not teach a specific Do/Dn ratio.

22. Chau further teaches "the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole" (column 6, lines 3-6). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Do/Dn ratio to give a desired draw ratio for the purpose of controlling the diameter of the filaments. It has been held that where the general conditions of a claim are disclosed in the prior art, discovering the optimum or workable ranges involves only routine skill in the art. *In re Aller, 105 USPQ 233, 235.*

23. With respect to claims 7 and 8, Kavesh as applied above teaches that the spinneret holds 28 should have a tapered entry region 30 followed by a capillary region of constant cross section 32 in which the length/diameter (L/D) ratio is more than about 10:1" (column 4, lines 50-53). In addition, Chau further teaches that the spinholes contain "(c) a capillary section (9), which is the thinnest (smallest-diameter) section of the hole where th walls are about parallel" (column 5, lines 36-38, figure 1) and "the

length of the capillary section is ... preferably at least about 0.1 times the diameter of the capillary... nor more than about 10 times the diameter of the capillary" (column 5, lines 45-53). It has been held that where the claimed range overlaps or lies inside of a prior art range a prima facie case of obviousness exists. *See In re Werthim, 541 F2d 257, 191 USPQ 90 (CCPA 1976).*

24. With respect to claim 10, the combination does not teach that the Lo/Do ratio of the constant diameter zone is at least 10.

25. Chau further teaches "the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole" (column 6, lines 3-6). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio of the constant diameter zone for the purpose of maximizing flow stability. It has been held that where the general conditions of a claim are disclosed in the prior art, discovering the optimum or workable ranges involves only routine skill in the art. *In re Aller, 105 USPQ 233, 235.*

26. With respect to claim 11, Chau further teaches:

wherein the spinplate comprises at least 10 cylindrical spinholes ("the spinneret may contain as many as 100 or 1000 or more" spinholes, column 5, lines 25-26), and wherein each cylindrical spinhole includes an inflow zone of constant diameter Do and a length Lo ("each hole contains (a) an inlet (1)", column 5, lines 31-32, figure 1) ..., a downstream zone of constant diameter Dn and a length Ln ("a capillary section (9)", column 5, line 36, figure 1) with a length/diameter ratio Ln/Dn of at most 15 (the length of the capillary is preferably nor more than about 10 times the diameter of thee capillary", column 5, lines 50-52), and a contraction zone between the inflow and downstream zones having a gradual decrease in diameter from the diameter Do to the diameter Dn with a cone angle in the range of 10-60° ("the angle must be no more than about 60", column 6, lines 49-50).

27. The combination does not teach that the Lo/Do ratio of the constant diameter zone is at least 10.

28. Chau further teaches "the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole" (column 6, lines 3-6). It would have been obvious to one of ordinary skill in the art at the time of the invention to optimize the Lo/Do ratio of the constant diameter zone for the purpose of maximizing flow stability. It has been held that where the general conditions of a claim are disclosed in the prior art, discovering the optimum or workable ranges involves only routine skill in the art. *In re Aller, 105 USPQ 233, 235.*

29. With respect to claim 12, the combination as applied to claim 1 above teaches DRsp's greater than 1.

30. Chau further teaches that "very high spin-draw ratios (such as 75, 100, 150 or 200 ore more) may be desirable" (column 7, line 68 to column 8, line 1) for the purpose of "spinning low diameter filaments using large holes" (column 7, lines 67-68).

31. It would have been obvious to one of ordinary skill in the art at the time of the invention that the combination teaches a range of DRfluid values which includes the claimed range of at least 100 for the purpose of producing low diameter fibers with a spinneret with large holes. Further more it has been held that where the claimed range overlaps or lies inside of a prior art range a prima facie case of obviousness exists. *See In re Werthim, 541 F2d 257, 191 USPQ 90 (CCPA 1976).*

32. With respect to claim 13, Kavesh further teaches:

Spinning a 3-15 mass% solution ("12 wt% linear polyethylene", column 5, line 55) of linear UHPE of IV 15-25 dl/g ("the linear poluethylene was himont UHMW 1900 having an intrinsic viscosity of 18 dl/g", column 6, lines 1-2) through a spinplate containing at least 10 spinholes ("feed the polymer solution ...to a 16-hole spinneret", column 6, line 6-7) into an air-gap ("passed through a spin gap", column 6, lines 11-12), ... and a draw ratio DRsolid of between 10

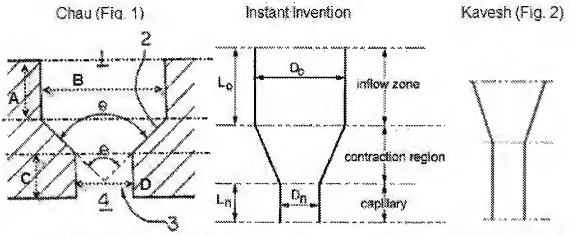
and 30 (see "solid state stretch" Table 1).

33. The spinhole geometry as instantly claimed is obvious over the combination as explained in the rejection of claim 11.

(10) Response to Argument

Applicant's arguments in the Appeal Brief filed 07/08/2011 have been fully considered but they are not persuasive.

34. Examiner provides the annotated figure below, which compares the instantly claimed geometry to the geometry of Kavesh and Chau, which are applied above, as a reference for the following discussion.



Note: The instant specification does not include a figure of the instantly claimed spinhole geometry. This figure is adapted from one presented in the Appeal Brief.

35. **With respect to the rejection of claims 14 and 15**, Applicant argues that Chau (Figure 3) does not teach an inflow zone with a length and thus can not teach the optimization of a length to diameter ratio of an inflow zone (Page 18 of the instant Brief).

36. Examiner finds this argument to be unpersuasive. Chau, as disclosed by figure 1, clearly contemplates an inlet zone with a discernable length (denoted as “A” in the annotated figure above). The fact that Figure 3 of Chau includes embodiments which do not have substantial inlet zones does not negate the disclosure of Figure 1. It has been held that disclosed examples and preferred embodiments do not constitute a teaching away from a broader disclosure or non-preferred embodiment. (*In re Susi*, 169 USPQ 423) Also, it has been held that a reference is not limited to its preferred embodiment, but must be evaluated for all of its teachings, including its teachings of non-preferred embodiments. (*In re Burckel,* 201 USPQ 67)

37. With respect to the rejection of claims 14 and 15, Applicant further argues that because Honnaker teaches that product properties are controlled by capillary dimensions one would "not include a counterbore, let alone optimize the counterbore dimensions when starting from the spinhole as disclosed by Chau" (page 19 of instant Brief).

38. Examiner finds this argument to be unpersuasive. The alleged intended use of the counterbore taught by Honnaker is not a limiting feature. Chau as applied in the rejection teaches a spinhole with the generally claimed shape and teaches that it is known to optimize the geometry. Honnaker teaches that spinholes with counterbores having the instantly claimed length/diameter ratio are known. It has been held that the combination of familiar elements according to known methods is likely to be obvious when it does not more than yield predictable results. *KSR Int'l Co. v. Teleflex Inc.,* 82 USPQ2d 1385 (2007).

39. **With respect to the rejection of claim 1**, Applicant argues that the spinhole taught by Kavesh "does not have a contraction region as is defined in the pending claims herein – it only has an entry region" (page 12 of the instant Brief).

40. Examiner finds this argument to be unpersuasive. This statement has been previously addressed in both the Non-Final Office Action (03/18/2010) and the Final Office Action (11/08/2010). The examiner's reasoning is duplicated below for completeness.

41. A contraction zone is defined in instant claim 1 as "having a gradual decrease in diameter from a diameter Do to a diameter Dn and a cone angle in the range from 8-75o". Examiner considers that Figure 2 of Kavesh (also replicated in the figure above) clearly shows a spinhole with an initial diameter and a gradual decrease in diameter to a smaller diameter capillary region. Regardless of what one chooses to name this zone, it meets the claim limitations of having an initial diameter which is greater than the final diameter and thus is sufficient to obviate a contraction zone as instantly claimed.

42. Applicant further argues that Kavesh does not contemplate drawing in the spinholes (DRsp) as instantly claimed (page 10 of the instant Brief).

43. Examiner finds this argument to be unpersuasive. The instant claims require a "DRsp being greater than 1" where the specification defines DRsp as (Do/Dn)2. Kavesh, as applied in the patentability analysis above, teaches that "the spinneret holes 28 should have a tapered...region" (column 4, lines 50-51) which examiner understands to mean than Do is required to be greater than Dn (see also Figure 2). Since Do is greater than Dn, the ratio of Do/Dn must be greater than 1. Squaring a number which is greater

than 1 will inherently result in an answer greater than 1. Thus the DRsp of Kavesh is inherently greater than 1.

44. With respect to the combination of Kavesh and Chau, applicant further argues that “the skilled person could not arbitrarily modify the inlet of Kavesh to also have the inlet (1) of Chau upstream of the inlet of Kavesh” without resulting in a spinhole with two constant diameter section (page 13 of instant Brief).

45. Examiner finds this argument to be unpersuasive. Kavesh teaches a 2 zone spinhole (figure 2). Chau teaches a 3 zone spinhole (figure 1). Examiner maintains that it would have been obvious to one of ordinary skill in the art at the time of the invention to modify the method and spin plate taught by Kavesh by adding an extended inlet section as taught by Chau to form a 3 zone spinhole for the purpose of maximizing the stability of polymer flow through the holes (Chau, column 6, lines 4-5).

46. Applicant further argues that Chau discloses a ratio of Lo/Do which is less than 1, not at least 5 as instantly claimed (page 13, instant Brief).

47. Examiner finds this argument to be unpersuasive. First, examiner notes that unless specifically indicated in a specification, drawings are not considered to be to scale and thus arguments based on the measurement of drawing features is of little value. (see *Hockerson-Halberstadt, Inc v. Avia Group Int'l*, 55 USPQ2d 1487, 14491). Furthermore, as applied in the patentability analysis above, Chau teaches “the size and geometry of the hole are preferably selected to maximize the stability of the dope flow through the hole” (column 6, lines 3-5). Thus it would have been obvious to one of ordinary skill in the art to optimize all features of spinhole geometry including Lo/Do.

48. Examiner also wishes to point out that the rejection is made optionally in view of Honnaker, which teaches a Lo/Do ratio of 2 to 8 (column 4, lines 6-9). One cannot show nonobviousness by attacking references individually where the rejections are based on combinations of references. See *In re Keller*, 642 F.2d 413, 208 USPQ 871 (CCPA 1981); *In re Merck & Co.,* 800 F.2d 1091, 231 USPQ 375 (Fed. Cir. 1986).

49. Applicant further argues that the combination of Kavesh and Chau can not meet the limitations regarding cone angle and DRfluid based upon a series of calculations (pages 14-16, instant Brief).

50. Examiner finds this argument to be unpersuasive. All of the calculations are based upon the assumption that Kavesh does not teach a contraction zone because only the dimensions of the capillary zone are specifically disclosed. Since the examiner considers that Kavesh does teach a contraction zone, as per paragraphs 40 and 41 above, the calculations provided by the applicant are not considered persuasive. As stated in the patentability analysis above, the combination of Kavesh and Chau meets all the limitations of the instant claims.

51. Finally, applicant argues that Kavesh can not be combined with Chau and/or Honnaker because they teach the spinning of different materials.

52. Examiner finds this argument to be unpersuasive. It has been held that a prior art reference must either be in the field of applicant's endeavor or, if not, then be reasonably pertinent to the particular problem with which the applicant was concerned, in order to be relied upon as a basis for rejection of the claimed invention. See *In re Oetiker*, 977 F.2d 1443, 24 USPQ2d 1443 (Fed. Cir. 1992). In this case, the instant

application relates to spinning a polymer with a viscosity of between 5 and 40 dl/g (claim 1, part “a)”). Kavesh teaches the spinning of polymers with a viscosity between about 4 dl/g and 40 dl/g (column 1, lines 40-41). Chau teaches spinning polymers with viscosities ranging between at least about 5 dl/g to preferably no more than about 50 dl/g (column 4, lines 18-32). Thus the examiner considers that they are all within the same field of endeavor. Honnaker also relates to the field of polymer spinning.

(11) Related Proceeding(s) Appendix

No decision rendered by a court or the Board is identified by the examiner in the Related Appeals and Interferences section of this examiner’s answer.

For the above reasons, it is believed that the rejections should be sustained.

Respectfully submitted,

/ALISON HINDENLANG/

Examiner, Art Unit 1744

Conferees:

/Anthony McFarlane/

/YOGENDRA GUPTA/

Supervisory Patent Examiner, Art Unit 1744